

Phase behavior of hard cylinders

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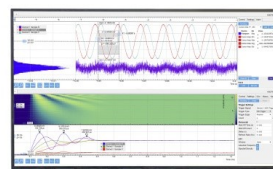
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ABSTRACT

Using isobaric Monte Carlo simulations, we map out the entire phase diagram of a system of hard cylindrical particles of length (L) and diameter (D) using an improved algorithm to identify the overlap condition between two cylinders. Both the prolate $L/D > 1$ and the oblate $L/D < 1$ phase diagrams are reported with no solution of continuity. In the prolate $L/D > 1$ case, we find intermediate nematic N and smectic SmA phases in addition to a low density isotropic I and a high density crystal X phase with I–N–SmA and I–SmA–X triple points. An apparent columnar phase C is shown to be metastable, as in the case of spherocylinders. In the oblate $L/D < 1$ case, we find stable intermediate cubatic (Cub), nematic (N), and columnar (C) phases with I–N–Cub, N–Cub–C, and I–Cub–C triple points. Comparison with previous numerical and analytical studies is discussed. The present study, accounting for the explicit cylindrical shape, paves the way to more sophisticated models with important biological applications, such as viruses and nucleosomes.

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I. INTRODUCTION

After nearly one century since Onsager's pioneering prediction that orientational order can be entropically induced for elongated particles,¹ simple models of rod-like objects continue to play a central role in the study of colloidal liquid crystals^{2,3} and self-assembly processes.^{4,5}

The simplest model for a rod-like molecule is the hard spherocylinder, an object formed by a cylinder of length L capped with two hemispheres of matching diameter D . This shape can be obtained by rolling a sphere of radius $D/2$ around a segment of length L . The great advantage of this model, and the key to its popularity, is the simplicity of the overlap condition between two such hard spherocylinders; this condition can be cast in a simple analytical form^{6,7} that can be computed very efficiently. As early as 1997, Bolhuis and Frenkel⁸ performed a remarkably detailed study of the phase

diagram of this model that is now considered a classic reference in the field. Other similar shapes have also been proposed in the literature, including hard ellipsoids,⁹ hard helices,¹⁰ and hard dumbbells.¹¹

However, there are physically relevant objects whose shape cannot be represented as hard spherocylinders but rather as hard cylinders (HCs). Examples include biologically relevant cases such as viruses^{3,12,13} and nucleosomes.^{14,15} Hard cylinders of length L and diameter D also have the additional advantage of having a natural oblate limit $L/D < 1$, approaching a disk for $L/D \rightarrow 0$, as well as the prolate limit $L/D > 1$ (rod). This is not the case of hard spherocylinders where the oblate limit is obtained by resorting to a slightly modified model.⁸ By contrast, the overlap condition between two cylinders is significantly more evolved with respect to the spherocylinder case. This notwithstanding, and given the similarity in shape, one might rightfully wonder what are the differences, if any,

in the two phase diagrams. For instance, the phase diagram of hard ellipsoids¹⁶ is different from the phase diagram of hard spherocylinders, in spite of the significant similarities in their shapes. This issue goes far beyond a simple academic problem in view of the strong propensity of nucleosomes^{14,15} and filamentous viruses^{17,18} to form a columnar phase, whose existence in the phase diagram of spherocylinders has been ruled out by recent detailed numerical simulations¹⁹ for prolate particles even if it were predicted theoretically²⁰ for oblate ones.

The aim of the present paper is to tackle this issue by performing a detailed analysis of the phase diagram of hard cylinders both in the prolate ($L/D > 1$) and in the oblate ($L/D < 1$) cases. While simulations of hard cylinders have been performed in the past,^{6,21,22} to the best of our knowledge our study is the first one providing the complete phase diagram. For this purpose, we perform isobaric Monte Carlo (MC) simulations of a system of hard cylinders in a wide range of aspect ratios L/D and volume fractions using an efficient method for the overlap test that compares well with the existing ones.^{6,21,22} The algorithm, inspired by Ref. 22, is described in the Appendix. By monitoring the appropriate order parameters and correlation functions, we provide the corresponding phase diagram in the L/D volume fraction plane and compare it with the corresponding phase diagram of the hard spherocylinders.⁸ Particular care has been devoted to avoiding possible finite size effects along the lines of a recent similar analysis for spherocylinders.¹⁹

The outline of this paper is as follows. In Sec. II, we described the details of our numerical approach, as well as the arsenal of tools (order parameters and correlation functions) useful to identify all different phases. Some technical details have been confined to the Appendix. Section III reports the main results of the present study with additional figures and tables given in the supplementary material. Finally, Sec. IV discusses the key messages of this study and some interesting perspectives for the future.

II. SIMULATIONS

A. Monte Carlo simulations

Our particles consist of N cylinders/disks of height L , diameter D , and whose orientations are identified by a unit vector $\hat{\mathbf{u}}$, as shown in Fig. 1(a). Pressures are measured in reduced units $P^* = P v_{\text{HC}} / k_B T$, and the density $\rho = N/V$ is represented by the volume fraction $\eta \equiv N v_{\text{HC}} / V$, where $v_{\text{HC}} = L \pi D^2 / 4$ is the volume of a hard cylinder (HC). We then performed isobaric (NPT) Monte Carlo (MC) simulations at different aspect ratios L/D both for rods ($L/D > 1$) and disks ($L/D < 1$). All simulations were organized in cycles (MC steps), each consisting, on average, of 1000 attempts to translate and rotate a randomly selected particle, and one attempt to change the volume of the simulation box. In all cases, we have performed compression runs starting at low pressure in the isotropic phase, and an expansion run starting from a close-packed solid configuration at high pressure. Each system was first equilibrated using $\approx 5.45 \times 10^6$ MC steps, with additional production runs of 1.5×10^5 steps. The typical number of particle was $N \approx 1000$, but different numbers were used depending on the aspect ratio, as detailed in Tables I and II. In the case of disks, the number of particles N was adjusted depending on L/D to keep the simulation box roughly cubic. In our NPT simulations, we have used floppy (i.e., shape-adapting) rectangular

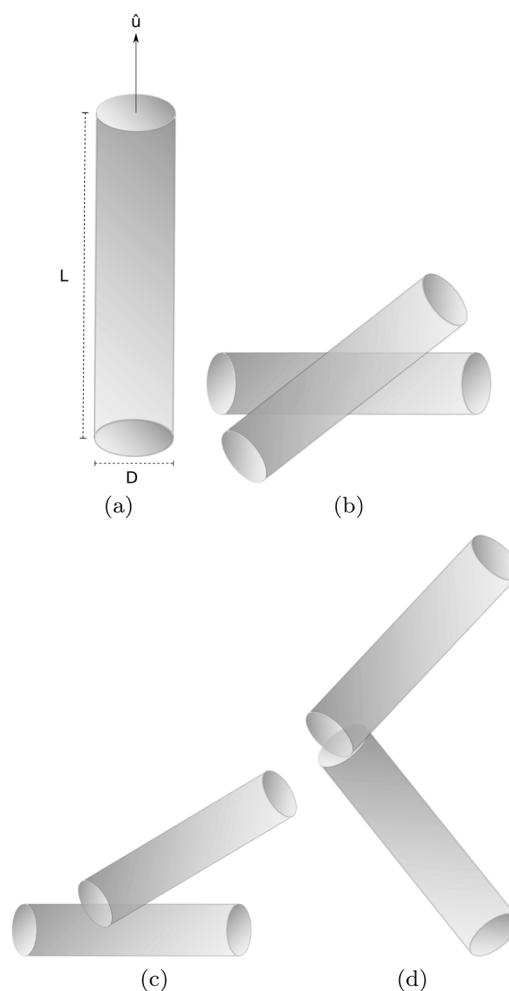


FIG. 1. (a) Our cylinder model, where L is the height, D is the diameter, and $\hat{\mathbf{u}}$ is the unit vector defining the orientation of the cylinder; possible overlap configurations between two cylinders (see the Appendix): (b) rim-rim; (c) rim-disk; and (d) disk-disk.

computational box, where one axis was randomly selected and its length was allowed to change with periodic boundary conditions to obtain an isotropic pressure⁸ in the prolate $L/D > 1$ case, and a simple uniform volume move with cubic periodic boundary conditions in the oblate $L/D < 1$ case. In some specific cases, we have also

TABLE I. Number of particles N used in the simulations of rods.

L/D	N	L/D	N
2.5	968	6.25	1350
3.0	1152	6.5	1350
3.25	1152	7.0	1536
3.5	1352	7.5	1536
5.0	1176	10.0	1944
6.0	1350		

TABLE II. Number of particles N used in the simulations of disks.

L/D	N	L/D	N
0.05	540	0.2	625
0.1	640	0.25	864
0.11	576	0.3	720
0.12	528	0.35	612
0.125	528	0.5	686
0.15	825		

extended the computational box along the main axis of the cylinders to minimize finite size effects.¹⁹

B. Overlap of hard cylinders

The first method for testing overlaps of hard cylinders was proposed by Allen *et al.*⁶ and also used by Blaak, Frenkel, and Mulder.²¹ An alternative method was recently proposed by Orellana, Romani, and De Michele.²² In the following, we use a refined version of this method outlined below. The overlap of two cylinders can occur in either of the following three ways: disk–rim, rim–rim, and disk–disk (Fig. 1). Therefore, to ensure that the cylinders do not overlap, we have to check whether the overlap occurs in one of those possible configurations, as detailed in the Appendix.

Preliminary simulations were initially performed to assess the computational effort of this algorithm compared with the hard spherocylinders counterpart. We found the present algorithm to be slightly slower, of the order of 20% or less, and hence in line with Ref. 22.

We perform the less expensive test first and progressively include additional more expensive ones. So, we first check whether the two spheres (of diameter $L + D$) that encompass the cylinders overlap; if they do not, the cylinders cannot overlap. If the encompassing spheres do overlap, the test is repeated for the spherocylinders enclosing the particles, using the standard algorithm to calculate the shortest distance between two rods.⁷ Only if the spherocylinders overlap, the overlap between two cylinders is tested for. See the Appendix for additional details.

C. Order parameters

To identify different thermodynamic phases, we rely on information based on global orientational and translational order, i.e.,

the nematic, smectic, and hexatic order parameters, on correlation functions such as the radial $g(\mathbf{r})$, parallel $g_{\parallel}(r_{\parallel})$ and perpendicular $g_{\perp}(r_{\perp})$ distribution functions, as well as on the visual inspection of the simulation snapshots. Figure 2 displays representative snapshots of all different phases obtained in the $L/D = 10$ —all snapshots were obtained using the Ovito Software²³ where different colors represent different orientations of cylinders. While the isotropic I phase is both positionally and orientationally disordered, the nematic N phase is positionally disordered but orientationally ordered, and its presence can be inferred monitoring the nematic order parameter P_2 . This is obtained as the largest eigenvalue of the tensor

$$Q_{\alpha\beta} = \frac{1}{N} \sum_{i=1}^N \frac{3}{2} \hat{\mathbf{u}}_{\alpha}^i \hat{\mathbf{u}}_{\beta}^i - \frac{1}{2} \delta_{\alpha\beta}, \quad (1)$$

where $\alpha, \beta = x, y, z$. The corresponding eigenvector then gives the main director $\hat{\mathbf{n}}$.

In addition to the orientational order along one preferred direction $\hat{\mathbf{n}}$, the smectic phase SmA is further characterized by a one-dimensional ordering (layering) along $\hat{\mathbf{n}}$ that is best captured by a combination of the radial distribution function

$$g(r) = \frac{1}{N\rho} \frac{1}{4\pi r^2} \left\langle \sum_{i=1}^N \sum_{j \neq i}^N \delta(r - r_{ij}) \right\rangle \quad (2)$$

and the parallel

$$g_{\parallel}(r_{\parallel}) = \frac{1}{N} \left\langle \frac{1}{\rho L_x L_y} \sum_i \sum_{j \neq i}^N \delta(r_{\parallel} - \mathbf{r}_{ij} \cdot \hat{\mathbf{n}}) \right\rangle \quad (3)$$

positional correlation function. Here, $\mathbf{r}_i$ is the center of mass of the i -th cylinder, $\mathbf{r}_{ij} = \mathbf{r}_j - \mathbf{r}_i$, and $r_{ij} = |\mathbf{r}_{ij}|$. The smectic order parameter

$$\langle \tau_1 \rangle = \left| \left\langle e^{i2\pi \frac{\mathbf{r} \cdot \hat{\mathbf{n}}}{d}} \right\rangle \right| \quad (4)$$

also proves convenient. Here, $\mathbf{r}$ is the position of a particle's center of mass and d is the optimal layer spacing. Here and below, $\langle \dots \rangle$ is the average over independent configurations at equilibrium. Then, we have $\langle \tau_1 \rangle \approx 1$ in the smectic SmA phase and $\langle \tau_1 \rangle \approx 0$ elsewhere (phases with no layered structure).

By contrast, the columnar C phase is characterized by two-dimensional in-plane hexagonal order and one-dimensional positional disorder along $\hat{\mathbf{n}}$. This is best captured by the perpendicular positional correlation function

$$g_{\perp}(r_{\perp}) = \frac{1}{2\pi r_{\perp} N} \left\langle \frac{1}{\rho L_z} \sum_i \sum_{j \neq i}^N \delta(r_{\perp} - |\mathbf{r}_{ij} \times \hat{\mathbf{n}}|) \right\rangle, \quad (5)$$

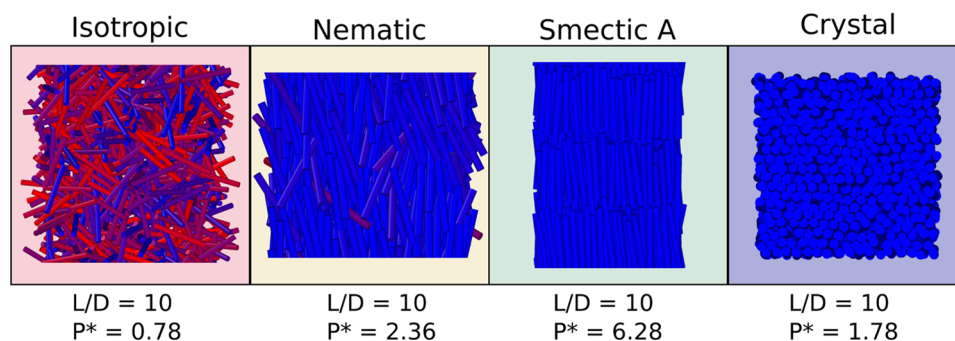


FIG. 2. Representative snapshots of the thermodynamic phases found for HC for $L/D = 10$: isotropic (I), nematic (N), smectic A (SmA), and crystal (X). Reduced corresponding pressures P^* are displayed.

positional correlation functions, as well as by the use of the hexatic (or bond) order parameter

$$\langle \psi_6 \rangle = \left\langle \frac{1}{N} \sum_j \left| \frac{1}{n(j)} \sum_{\langle lm \rangle} e^{6i\theta_{lm}} \right| \right\rangle. \quad (6)$$

Here, θ_{lm} is the angle that the projection of the intermolecular vectors $\mathbf{r}_{jl}$ and $\mathbf{r}_{jm}$ onto the plane perpendicular to the director $\hat{\mathbf{n}}$, $n(j)$ is the number of nearest-neighbors pairs of molecule within a single layer, and the sum $\sum_{\langle lm \rangle}$ is over all possible pairs within the first coordination shell. With this definition, $\langle \psi_6 \rangle \approx 1$ for hexagonal in-plane ordering and $\langle \psi_6 \rangle \approx 0$ otherwise. We refer to the past literature (see, e.g., Kolli *et al.*²⁴ and references therein) for additional details.

Finally, the cubic Cub phase corresponds to a long-range orientationally ordered phase without any positional order but with the presence of three equivalent perpendicular directions. In this phase, the particles form short stacks of typically few particles with neighboring stacks tending to be perpendicular to one another along the three selected directions. While a suitable order parameter can be devised,²⁵ visual inspection is usually sufficient to unambiguously identify this phase. The details of the cubic Cub phase will be discussed in Sec. III.

III. RESULTS

A. Cylindrical rods $L/D > 1$

We first consider the prolate case, i.e., cylindrical rods with $L/D > 1$. Figure 3(a) depicts the reduced pressure P^* as a function of the volume fraction η (i.e., the equation of state) for $L/D = 5$ and $L/D = 10$. Figure 3(b) shows also the corresponding orientational order parameter P_2 again as a function of the volume fraction η .

In the case $L/D = 5$ (open symbols), the system is in an isotropic phase I until $\eta \approx 0.4$, then switches to a smectic SmA phase, and then to a crystal X phase. The same sequence of phases is also found for the large aspect ratio $L/D = 10$ (closed symbols) but with transitions shifted to lower η and with the additional presence of a nematic N phase in the region $0.3 \leq \eta \leq 0.4$. The isotropic–nematic transition is signaled by an abrupt jump in the nematic order parameter P_2 as shown in Fig. 3(a).

Here, it is worth to notice that our definition of crystal phase X includes the so-called smectic SmB phase, another name often used in this framework,²⁴ that is, a smectic SmA phase with additional in-plane long-range hexagonal order,³ thus hardly distinguishable from a crystal phase due to the finite size of the simulations box.

Additional insights can be obtained by looking at the correlation functions at an intermediate aspect ratio $L/D = 7$ —see [supplementary material](#) Fig. S1 for the analog of Fig. 3 in the case $L/D = 7$. Figure 4 presents the corresponding radial $g(r)$ (a), parallel $g_{\parallel}(r_{\parallel})$ (b), and perpendicular $g_{\perp}(r_{\perp})$ (c) distribution functions of cylinders with $L/D = 7$ for increasing pressures.

At $P^* = 3.96$ (continuous red line), all correlation functions are featureless, indicating the presence of an isotropic I phase. As pressure is increased up to $P^* = 4.40$ (yellow dashed line), the correlation functions do not show any significant change but the nematic order parameter P_2 [see the [supplementary material](#), Fig. S1(b)] shows an abrupt upswing, signaling the onset of a nematic N phase.

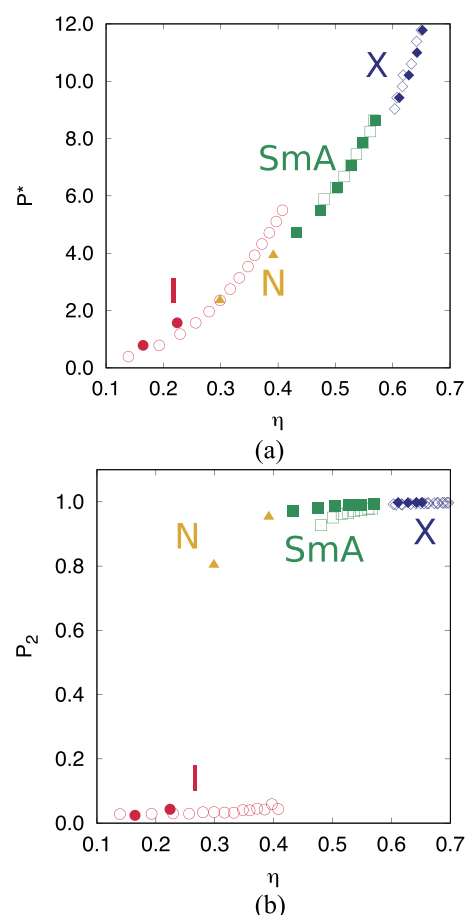
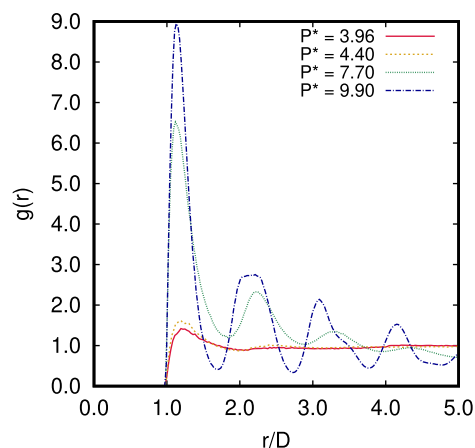


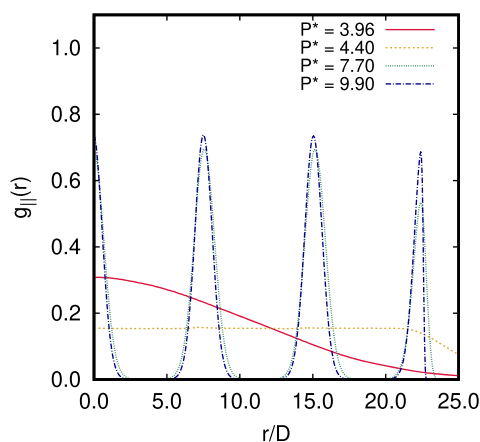
FIG. 3. (a) Reduced pressure P^* vs cylinder volume fraction η . Open symbols: $L/D = 5$ and closed symbols: $L/D = 10$; (b) nematic order parameter P_2 vs volume fraction η for both $L/D = 10$ and $L/D = 5$. Same symbols as above. The different symbols and colors refer to different mesophases, as detailed in Fig. 2.

At $P^* = 7.70$ (green dotted line), both the radial distribution function $g(r)$ and the parallel correlation function $g_{\parallel}(r_{\parallel})$ display a clear periodicity consistent with a smectic SmA ordering. The absence of regular oscillations in the perpendicular correlation function $g_{\perp}(r_{\perp})$ confirms the radial liquid-like order of the mesophase, which, therefore, does not correspond to the crystal X phase. The latter phase is eventually reached at $P^* = 9.90$ (dashed-dotted line) as shown by the characteristic periodicities for all directions in $g_{\perp}(r_{\perp})$ as well as in $g(r)$ and $g_{\parallel}(r_{\parallel})$.

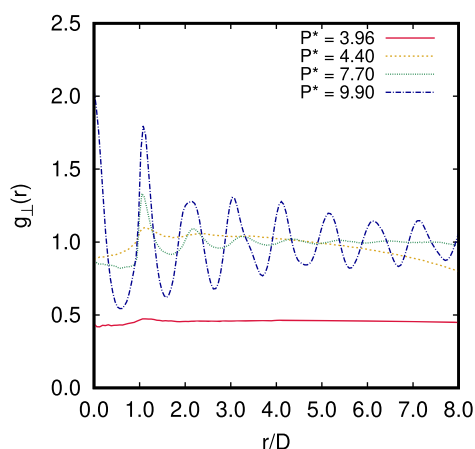
It comes as no surprise that the low- η behavior of HCs is qualitatively similar to the corresponding Hard SpheroCylinders (HSC) counterpart,⁸ with small quantitative differences for the smaller aspect ratio $L/D = 5$. However, at high pressure and volume fraction, one possible important element of distinction between the two phase diagrams is the presence of a putative columnar phase that has already been demonstrated not to exist in the HSC counterpart.¹⁹ We explicitly addressed this problem following the method proposed by Dussi, Chiappini, and Dijkstra¹⁹ who suggested that the apparent stabilization of a columnar phase in HSCs could be



(a)



(b)



(c)

FIG. 4. Distribution functions of cylinders with $L/D = 7.0$. $P^* = 3.96$ continuous red line (I); $P^* = 4.40$ yellow dashed line (N); $P^* = 7.70$ green dotted line (SmA); $P^* = 9.90$ dashed-dotted line (X). Note that $r = |r|$ in (a), $r = |r_{\parallel}|$ in (b), and $r = |r_{\perp}|$ in (c).

ascribed to finite size effects when the number of layers is not sufficiently high compared to the aspect ratio L/D . For sake of consistency, we first reproduced the same results found in Ref. 19 for HSCs, and then applied the same method to the HC case. We note that the metastability of the columnar phase for HSCs was also independently confirmed by Liu and Widmer-Cooper²⁶ using a different method.

The results obtained are presented in Fig. 5. Figure 5(a) shows a production run with aspect ratio $L/D = 6$ at packing fraction $\eta = 0.6$. In this case, both visual inspection and the behavior of the corresponding correlation functions (see the solid line in supplementary material, Fig. S2, for results with $N = 675$) strongly suggest the presence of a columnar phase. However, if the number of particles is doubled along the director $\hat{n}$, the same calculation produces the final configuration shown in Fig. 5(b) that can clearly be classified as smectic SmA (see the dotted line in supplementary material, Fig. S2, for results with $N = 1350$). This shows that there is no stable columnar phase in HCs as in the HSCs case. This effect is likely to be ascribed to the preference for finite size domains to arrange locally in columnar structures whose stability is eventually overwhelmed by long-range effects.

A sketch of the final phase diagram for HCs in the plane packing fraction η as a function of the aspect ratio ranging from $L/D = 2.5$ to 10 is displayed in Fig. 6. The color codes used to represent different phases are outlined in Fig. 2 that also presents representative snapshots of each phase. Here, we employ the same classification as Dussi, Chiappini, and Dijkstra.¹⁹

Similar to hard spherocylinders, the system exhibits the isotropic (I), nematic (N), smectic A (SmA), and crystalline (X) phases.

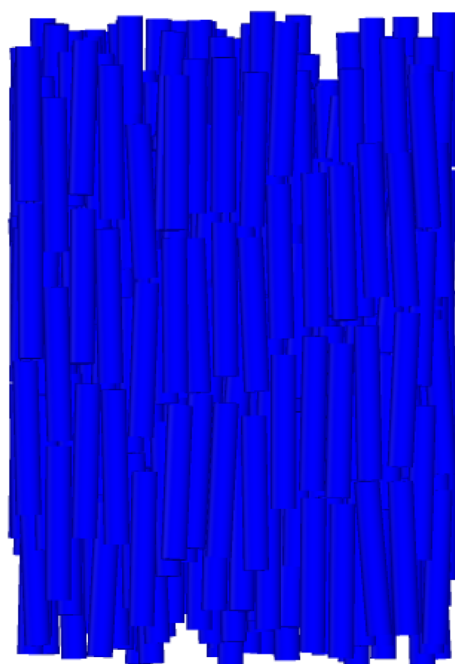
Not surprisingly, this behavior is similar to that of HSCs,^{8,27} but few differences are worth noticing.

As in the case of HSCs, no liquid crystal phases are observed below a critical aspect ratio $L/D \approx 3$. This fact can be easily rationalized via Onsager theory,¹ as the ratio between the covolume and volume of rods with lower L/D is not sufficiently larger than that of a sphere, and the excluded volume effects then are insufficient to promote an organized orientationally ordered phase. By contrast, at sufficiently high densities and aspect ratios, the excluded volume effects tend to promote orientational order to increase the translational entropy, and then minimizing the free energy.

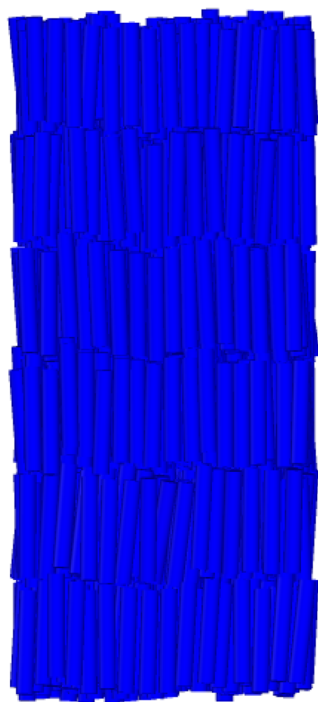
Accordingly, the system is in the isotropic phase for any ratio L/D below a certain packing fraction that decreases by increasing the rod aspect ratio, as shown in Fig. 6. Upon increasing η , the first organized phase encountered is a smectic SmA phase in the range from $L/D = 3.25$ to $L/D = 6$, and a nematic N phase above $L/D \approx 6$. This mirrors the HSC case where, however, the smectic SmA phase is limited to a very small range $3 < L/D < 4$. At higher packing fractions η , the system undergoes a smectic SmA to crystal X transition irrespective of the aspect ratio L/D .

The sketched phase diagram in Fig. 6 prompts the existence of an isotropic-smectic-solid (I-SmA-X) triple point at $\eta \approx 0.55$ and $L/D \approx 3.0$, and an isotropic-nematic-smectic (I-N-SmA) triple point at $\eta \approx 0.4$ and $L/D = 6.5$.

Interestingly, the location of the I-N-SmA is found at $L/D \approx 6.5$ and shifted to higher aspect ratios compared to that of HSCs, which is found at $L/D \approx 3.7$.⁸ As a result, the nematic N phase stabilizes at shorter aspect ratios in the HSC system when compared to its HC counterpart.



(a)



(b)

FIG. 5. Equilibrated configuration with aspect ratio $L/D = 6$ at packing fraction $\eta = 0.6$ with (a) $N = 675$ initially distributed on two layers. (b) The same result with twice the particles exhibits a different structure.

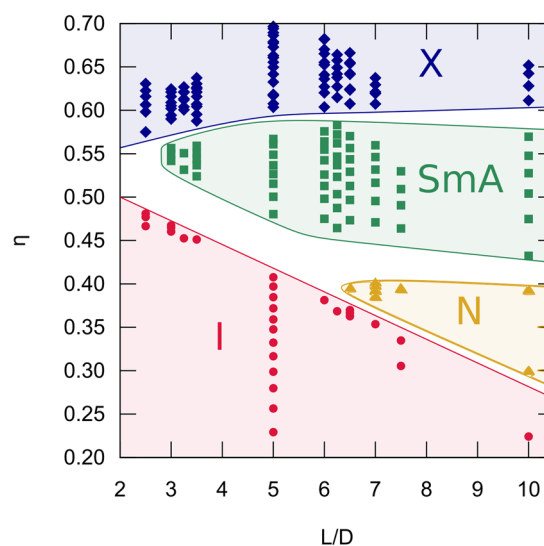


FIG. 6. Computed phase diagram of hard cylinders of packing fraction η vs aspect ratio L/D . Visible phases are isotropic (I), nematic (N), smectic (SmA), and crystal (X). Color codes are as in Fig. 2.

It is also interesting to notice that our results are compatible with both I–N and the N–SmA being first-order transitions, thus mirroring what is known for the HSC from the work by Polson and Frenkel.²⁸ It would be interesting to pursue the same analysis carried out by these authors in the present case as well. The same consideration holds true for an interesting analysis of the $L/D \rightarrow \infty$ Onsager limit that has been performed for the HSC case⁸ that could also be replicated in this case.

As a final remark, we note that the length L for HSCs corresponds to $L + D$ in the case of HCs. This is important when comparing the corresponding phase diagrams and, indeed, it rationalizes why the isotropic–smectic I–SmA transition for HCs occurs at $L/D \approx 3$ whereas for HSCs, it occurs at $L/D \approx 4$. However, the tendency of a flat edge to promote the onset of a smectic SmA phase appears to be a general feature as also suggested by a recent study²⁹ on hard equilateral triangular prisms, where the particles feature also flat sides and the smectic SmA phase is shifted to considerably lower packing fractions as compared to HSCs.

B. Cylindrical disks $L/D < 1$

We now tackle the oblate case of cylindrical disks with $L/D < 1$. One important advantage of dealing with cylinders is that this limit can be achieved with no solution of continuity, unlike the spherocylinders counterpart where this is not possible.⁸ Figure 7 depicts the four different phases that we find in this case: a disordered isotropic I, a cubatic Cub, a nematic N, and a columnar C phase, as detailed in Table III and illustrated in Fig. 7.

As in this case of prolate cylinders, we performed the same detailed analysis of the different obtained phases in terms of correlation functions and order parameters to derive the equation of states. Supplementary material Fig. S3 shows the reduced pressure P^* and the P_2 nematic order parameter as a function of the packing

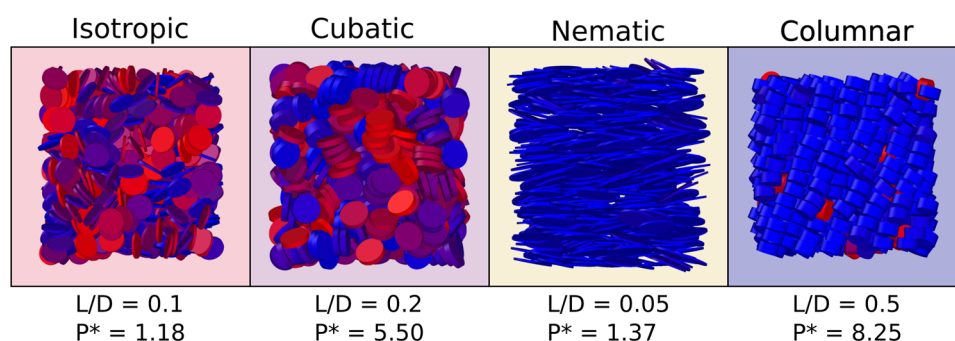


FIG. 7. Representative snapshots of the different phases found in the oblate $L/D < 1$ case: isotropic (I), cubatic (Cub), nematic (N), and columnar (C). The corresponding values of aspect ratios L/D and reduced pressure P^* are also reported.

fraction η for both $L/D = 0.2$ and $L/D = 0.05$ as representative examples, from which one can obtain the corresponding phase diagram of Fig. 8 in the volume fraction η aspect ratio L/D plane, which can be contrasted with its prolate counterpart shown in Fig. 6. Here, a range from $L/D = 0.05$ to $L/D = 0.5$ has been analyzed, and in Fig. 7, representative snapshots of different phases are depicted to be color-coded according to Table III, in analogy with the discussion of the prolate case $L/D > 1$.

For aspect ratios $0.3 < L/D < 0.5$, there is a direct transition from an isotropic I to a columnar C phase upon increasing η

TABLE III. Colors and symbols used to represent disk phases.

Color	Phase	Notation	Symbol
Red	Isotropic	I	Circle
Yellow	Nematic	N	Triangle
Purple	Cubatic	Cub	Squares
Blue	Columnar	C	Diamond

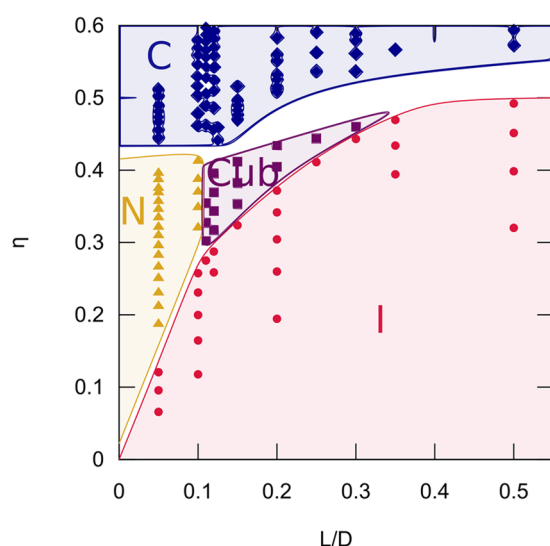


FIG. 8. Phase diagram of the oblate hard cylindrical disk case $L/D < 1$ in the volume fraction η aspect ratio L/D plane. Different phases are color coded as detailed in Fig. 7 and Table III.

above ≈ 0.4 . In the columnar phase, the disks are arranged on a hexagonal lattice in the direction perpendicular to the main director $\hat{n}$ but their centers of mass are disorderly distributed in space. For smaller aspect ratios $0.1 < L/D < 0.3$, a cubatic Cub phase appears between the I and C phase. In the cubatic phase, the disks tend to assemble in short stacks of about four or five units, with the neighboring columns perpendicular to each other. This differs from the cubic phase because it lacks translational order.³⁰ At even smaller aspect ratios ($L/D \leq 0.1$), the cubatic Cub phase is replaced by a nematic N phase up to $\eta \approx 0.4$ and by a columnar phase at higher η . At even higher packing fractions η , we did observe the formation of a crystal phase X, but the location of the corresponding boundaries would require a specific investigation that was not pursued in the present paper.

All these transitions can be best inferred by looking at the correlation functions as shown in Fig. 9 (see Fig. 7 for the corresponding snapshots). In the I phase (red continuous line), the radial distribution function $g(r)$ displays a flat behavior for $r > D$, indicating the absence of short-range aggregation, a feature confirmed by the behavior of both $g_{\parallel}(r_{\parallel})$ and $g_{\perp}(r_{\perp})$. By contrast, the columnar C phase (blue dashed line) displays characteristic regular oscillations in $g(r)$ and $g_{\perp}(r_{\perp})$, but the behavior of $g_{\parallel}(r_{\parallel})$ is irregular, indicating the absence of a one-dimensional ordering along the main director $\hat{n}$. Likewise, the radial distribution function $g(r)$ of the cubatic phase (dotted purple line) is quite different from both the I and C phases, while the nematic order parameter P_2 is close to zero for I and Cub. Evidence of the formation of short stacks is the higher peak at short distances ($L/D < r/D < 2L/D$) in the radial distribution function $g(r)$ of the cubatic Cub phase (the purple line in Fig. 9), which is significantly smaller in the $g(r)$ of an isotropic phase [the red line in Fig. 9(a)]. Finally, the onset of the nematic N phase (dashed-dotted yellow line) is signaled by the significant oscillation of the radial distribution function $g(r)$ and by the abrupt upswing in the nematic order parameter P_2 , as shown in the supplementary material.

At variance with the prolate $L/D > 1$ counterpart, in the oblate case, three triple points appear. The I–N–Cub triple point occurs at $L/D \approx 0.1$ and $\eta \approx 0.3$. The N–Cub–C triple point is approximately located at $L/D \approx 0.1$ and $\eta \approx 0.4$. Finally, the I–Cub–C triple point has approximate coordinates $L/D \approx 0.35$ and $\eta \approx 0.45$.

Our results qualitatively agree with the density function calculations by Wensink and Lekkerkerker²⁰ who predicted the existence of a nematic region for flat disks that becomes progressively narrower as L/D increases. The same authors also predicted a transition

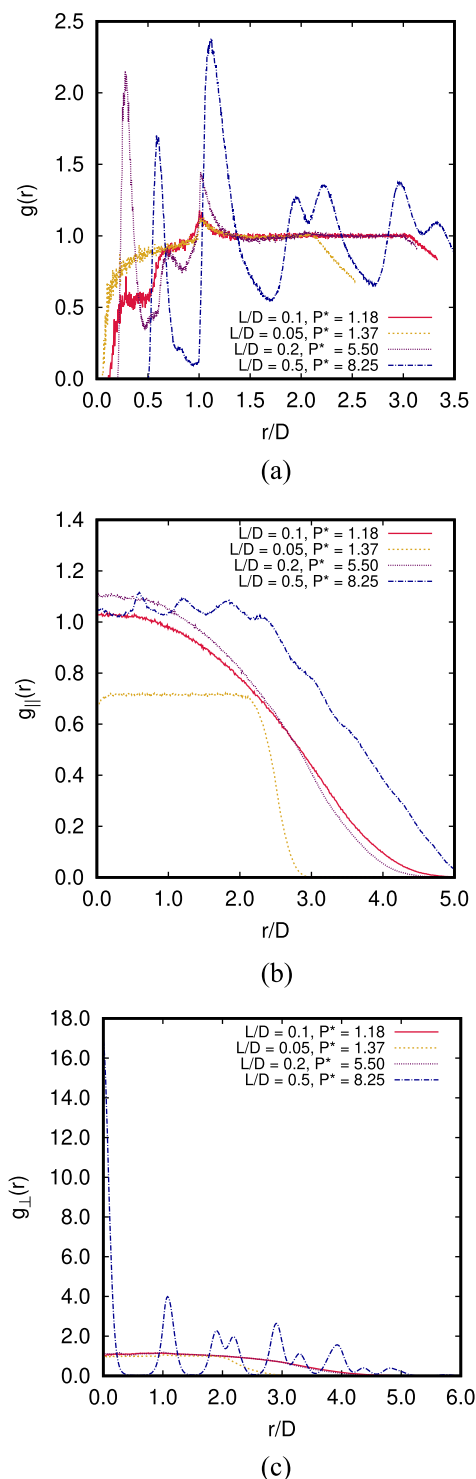


FIG. 9. Distribution functions of hard cylindrical disks. $L/D = 0.1$ and $P^* = 1.18$ red continuous line I; $L/D = 0.05$ and $P^* = 1.37$ blue dashed line C; $L/D = 0.2$ and $P^* = 5.50$ dotted purple line Cu; $L/D = 0.5$ and $P^* = 8.25$ dashed-dotted yellow line N. The color code is outlined in Table III. Here, again $r = |r|$ in (a), $r = |r_{\parallel}|$ in (b), and $r = |r_{\perp}|$ in (c).

from the isotropic phase directly to the columnar C phase, in agreement with our results. At a more quantitative level, the predicted volume fractions $\eta_{IN} \approx \pi L/D$ for the isotropic–nematic transition and $\eta_{NC} \approx 0.4$ for the nematic–columnar N–C, as somewhat larger than those found in the present study.

At variance of these theoretical findings, our results indicate also the existence of a cubatic Cub phase, in agreement with the results by Veerman and Frenkel,³⁰ as well as by Duncan *et al.*,²⁵ in simulations of cut spheres, and by Blaak, Frenkel, and Mulder²¹ in simulations of hard cylinders. Where direct comparison with the above two papers is possible, we find complete agreement between their results and ours.

Duncan *et al.*²⁵ simulated cut spheres of $L/D = 0.1, 0.15, 0.2, 0.25$, and 0.3 , and, despite the differences in shape, our results are very similar to theirs. These authors showed that there is a nematic N but no cubatic Cub phase at $L/D = 0.1$, and that the opposite is true for $L/D \geq 0.15$. Figure 8 shows that for HCs, a cubatic Cub phase is already present at $L/D = 0.11$, as the nematic N phase vanishes. The cubatic Cub phase is present until $L/D \approx 0.3$, whereas only the isotropic I and columnar C phases exist at larger aspect ratios.

As in our case, Blaak, Frenkel, and Mulder²¹ investigated a system of HC with $L/D = 0.9$ and did not find any cubatic phase. Our results explain this finding by showing that $L/D = 0.9$ is a too large aspect ratio to support a cubatic phase that is, however, present at a smaller aspect ratio $0.1 < L/D < 0.3$, as shown in Fig. 8.

IV. CONCLUSIONS

In this paper, we have used isobaric (NPT) Monte Carlo simulations to study the phase diagram of a system of N hard cylinders as a function of their aspect ratio and volume fraction. To achieve this, we have implemented a new and efficient overlap test for hard cylinders that compares well with those existing in the literature.^{21,22} This allows us to study the complete phase diagrams in the aspect ratio vs volume fraction for both the prolate $L/D > 1$ and the oblate $L/D < 1$ cases.

In the prolate case $L/D > 1$, we find a phase diagram very similar to the hard spherocylinders counterpart, featuring the presence of a nematic N and a smectic SmA phase, in addition to the isotropic I and the crystal X phases, as well as two I–Sm–X and I–N–SmA triple points. As in the spherocylinder case,¹⁹ we have shown that the appearance of a columnar C phase can be traced back to a finite-size effect and that it disappears for sufficiently large systems. Our simulations confirm the lack of existence of a stable columnar C phase, which was, nevertheless, predicted by density functional theory.²⁰

In the oblate case $L/D < 1$, we identified the presence of a columnar C, a nematic N, and a cubatic Cub phase, in agreement with theoretical prediction,²⁰ as well as with past numerical simulations of cut spheres^{25,30} and hard cylinders.²¹ In the latter case, we have provided an explanation of the failure of past simulations of identifying the cubatic Cub phase that can be ascribed to the too large aspect ratio used in these simulations. Interestingly, the phase diagram also includes three I–N–Cub, N–Cub–C, and I–Cub–C triple points.

This study paves the way to tackling more complex systems building upon cylindrical shapes that are of experimental interest, such as hard cylinders interacting via a Yukawa tail,³ as well

as hard cylinders with short-range directional attractions.^{15,31} Such investigations are underway and will be reported elsewhere.

SUPPLEMENTARY MATERIAL

See the [supplementary material](#) for additional figures and tables, including all relevant data reported in the manuscript.

ACKNOWLEDGMENTS

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APPENDIX: ALGORITHM TO CHECK OVERLAP BETWEEN TWO CYLINDERS

1. Parallel cylinders

If two cylinders are parallel, the overlap can occur between disk-disk or rim-rim only, and it can be easily checked. For each particle pair, we define four vectors starting from the vector joining the two centers of mass, $\mathbf{r}_{12}$. We do this by extracting its parallel and perpendicular component with respect to the director $\hat{\mathbf{u}}_j$ of each particle, i.e.,

$$\begin{aligned}\mathbf{r}_{1\parallel} &= (\mathbf{r}_{12} \cdot \hat{\mathbf{u}}_1) \hat{\mathbf{u}}_1, \\ \mathbf{r}_{2\parallel} &= (\mathbf{r}_{12} \cdot \hat{\mathbf{u}}_2) \hat{\mathbf{u}}_2, \\ \mathbf{r}_{1\perp} &= \mathbf{r}_{12} - (\mathbf{r}_{12} \cdot \hat{\mathbf{u}}_1) \hat{\mathbf{u}}_1, \\ \mathbf{r}_{2\perp} &= \mathbf{r}_{12} - (\mathbf{r}_{12} \cdot \hat{\mathbf{u}}_2) \hat{\mathbf{u}}_2.\end{aligned}\quad (\text{A1})$$

In a parallel configuration, the directors can either be the same or the opposite of the other. The overlap occurs if *all* the following conditions are satisfied:

$$\begin{aligned}|\mathbf{r}_{1\parallel}| &\leq L, \\ |\mathbf{r}_{2\parallel}| &\leq L, \\ |\mathbf{r}_{1\perp}| &\leq D, \\ |\mathbf{r}_{2\perp}| &\leq D.\end{aligned}\quad (\text{A2})$$

When the cylinders are *exactly* parallel, $\hat{\mathbf{u}}_1 = \pm \hat{\mathbf{u}}_2$, and half of the conditions above are redundant since $|\mathbf{r}_{1\perp}| = |\mathbf{r}_{2\perp}|$ and $|\mathbf{r}_{1\parallel}| = |\mathbf{r}_{2\parallel}|$; when implementing the computer code, however, one has to include tolerances and care must be taken in handling these conditions consistently.

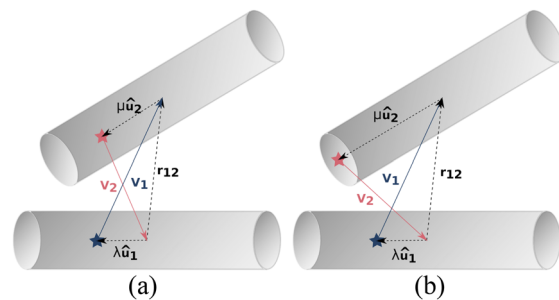


FIG. 10. The star symbols represent the points of closest approach on each cylinder. (a) Rim-rim configuration, (b) disk-rim configuration.

2. Rim-rim overlap

Since the overlap between spherocylinders is the first test that is done, and the rim of a spherocylinder is similar to the rim of a cylinder, if the rims of two spherocylinders do overlap, the two cylinders will certainly overlap as well. Hence, having performed the spherocylinder overlap test, we now check if the overlap occurs in a rim-rim configuration.

To that end, we define the vectors $\mathbf{V}_1 = -\mathbf{r}_{12} + \lambda \hat{\mathbf{u}}_1$ and $\mathbf{V}_2 = \mathbf{r}_{12} + \mu \hat{\mathbf{u}}_2$, where the numbers λ and μ , consistently with Ref. 7, identify the points of closest approach between the axes of the two cylinders. These values are calculated using the Vega and Lago's algorithm,⁷ which we implement in the spherocylinder overlap test. If the cylinders are in a rim-rim configuration, the two conditions below must be satisfied:

$$\begin{aligned}|\mathbf{V}_1 \cdot \hat{\mathbf{u}}_2| &< L/2, \\ |\mathbf{V}_2 \cdot \hat{\mathbf{u}}_1| &< L/2.\end{aligned}\quad (\text{A3})$$

In Fig. 10, we see that in the case of a disk-rim configuration, for instance, the projection of $\mathbf{V}_1$ in the direction of $\hat{\mathbf{u}}_2$ is larger than $L/2$.

3. Disk-disk overlap

The orientations of the cylinders are perpendicular to the planes of the disks. The planes of the two disks intersect in a line parallel to $\hat{\mathbf{u}}_1 \times \hat{\mathbf{u}}_2$. We define $\mathbf{P}_1$ and $\mathbf{P}_2$ as being the points in the intersection line that are closer to the disk centers $\mathbf{d}_1$ and $\mathbf{d}_2$, respectively, as shown in Fig. 11.

To find $\mathbf{P}_1$, we minimize $(\mathbf{P}_1 - \mathbf{d}_2)^2$, which is equivalent to minimizing $|\mathbf{P}_1 - \mathbf{d}_1|$. The minimization can be done by applying Lagrange multipliers with two constraints,

$$(\mathbf{P}_1 - \mathbf{d}_1) \cdot \hat{\mathbf{u}}_1 = 0, \quad (\text{A4a})$$

$$(\mathbf{P}_1 - \mathbf{d}_2) \cdot \hat{\mathbf{u}}_2 = 0. \quad (\text{A4b})$$

The constraints presented in Eq. (A13) ensure that $\mathbf{P}_1$ is in a line perpendicular to both $\hat{\mathbf{u}}_1$ and $\hat{\mathbf{u}}_2$. Applying the Lagrange multipliers,

$$\mathcal{L} = (\mathbf{P}_1 - \mathbf{d}_1)^2 - \lambda (\mathbf{P}_1 - \mathbf{d}_1) \cdot \hat{\mathbf{u}}_1 - \mu (\mathbf{P}_1 - \mathbf{d}_2) \cdot \hat{\mathbf{u}}_2. \quad (\text{A5})$$

From $\nabla \mathcal{L} = 0$, one has

$$\mathbf{P}_1 = \mathbf{d}_1 + \frac{\lambda \hat{\mathbf{u}}_1}{2} + \frac{\mu \hat{\mathbf{u}}_2}{2}. \quad (\text{A6})$$

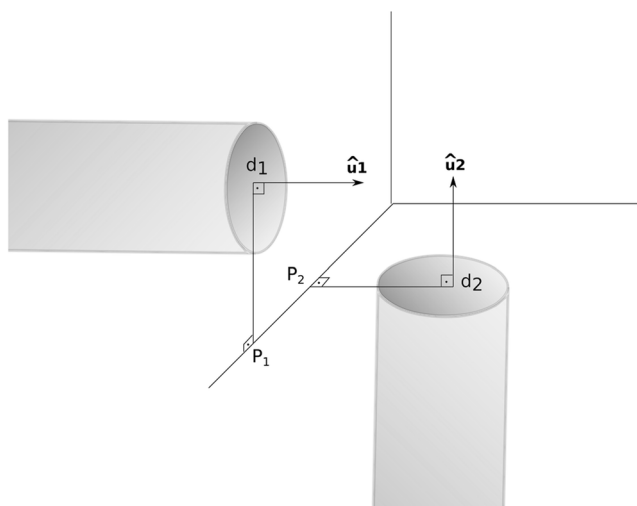


FIG. 11. Disks of two cylinders.

Replacing Eq. (A4a) into Eq. (A6) gives

$$\lambda = -\mu(\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2). \quad (\text{A7})$$

Substituting Eqs. (A4b) and (A7) into (A6) yields

$$\mu = \frac{-2(\mathbf{d}_1 - \mathbf{d}_2) \cdot \hat{\mathbf{u}}_2}{1 - (\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2)^2}. \quad (\text{A8})$$

Replacing Eq. (A8) into (A7) gives

$$\lambda = \frac{2[(\mathbf{d}_1 - \mathbf{d}_2) \cdot \hat{\mathbf{u}}_2] \cdot (\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2)}{1 - (\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2)^2}. \quad (\text{A9})$$

Replacing Eqs. (A8) and (A9) into (A6) gives

$$\mathbf{P}_1 = \mathbf{d}_1 + \frac{[(\mathbf{d}_1 - \mathbf{d}_2) \cdot \hat{\mathbf{u}}_2] \cdot ((\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2) \cdot \hat{\mathbf{u}}_1 - \hat{\mathbf{u}}_2)}{1 - (\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2)^2}. \quad (\text{A10})$$

We define $\mathbf{d}_{12} = \mathbf{d}_2 - \mathbf{d}_1$ and $\Delta_1^2 = (\mathbf{P}_1 - \mathbf{d}_1)^2$ and rewrite Eq. (A10) as

$$\Delta_1^2 = \frac{(\mathbf{d}_{12} \cdot \hat{\mathbf{u}}_2)^2 \cdot ((\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2)^2 - 2(\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2) + 1)}{(1 - (\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2)^2)^2}. \quad (\text{A11})$$

Simplifying Eq. (A11) gives

$$\Delta_1^2 = \frac{(\mathbf{d}_{12} \cdot \hat{\mathbf{u}}_2)^2}{1 - (\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2)^2}. \quad (\text{A12})$$

Similarly, for disk 2,

$$\Delta_2^2 = \frac{(\mathbf{d}_{12} \cdot \hat{\mathbf{u}}_1)^2}{1 - (\hat{\mathbf{u}}_1 \cdot \hat{\mathbf{u}}_2)^2}. \quad (\text{A13})$$

A necessary, but not sufficient, condition for the overlap to occur is that both Δ_1 and Δ_2 have to be less than the cylinder radius $D/2$. If this condition is satisfied, the intersection line crosses both disks through segments of length $2\delta_1$ and $2\delta_2$, as presented in Fig. 12.

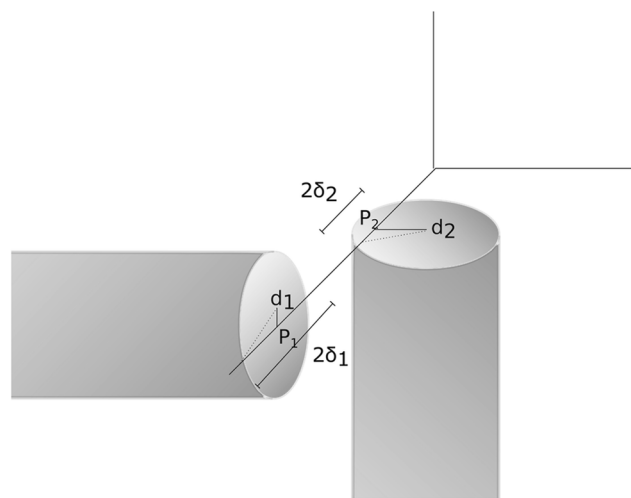


FIG. 12. Disks of two cylinders.

The expressions to calculate δ_1 and δ_2 are presented in the following equation:

$$\delta_1 = \sqrt{\frac{D^2}{4} - \Delta_1^2} \quad (\text{A14})$$

$$\delta_2 = \sqrt{\frac{D^2}{4} - \Delta_2^2}.$$

Finally, an overlap will occur if the condition in the following equation is true:

$$|\mathbf{P}_2 - \mathbf{P}_1| = \left| \mathbf{d}_{12} \cdot \frac{(\hat{\mathbf{u}}_1 \times \hat{\mathbf{u}}_2)}{|\hat{\mathbf{u}}_1 \times \hat{\mathbf{u}}_2|} \right| \leq \delta_1 + \delta_2. \quad (\text{A15})$$

4. Disk-rim overlap

Let us take a disk with center in $\mathbf{d}_j$ and a cylinder with center in $\mathbf{r}_i$ (Fig. 13). We define $\mathbf{U}_i$ as the point on cylinder i that is the closest

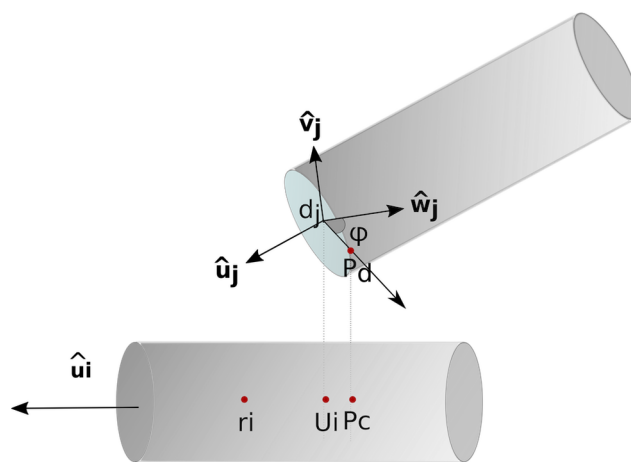


FIG. 13. Disk-rim configuration.

to $\mathbf{d}_j$, $\mathbf{P}_d$ a point on the disk j that is the closest to cylinder i , $\mathbf{P}_c$ a point on cylinder i that is the closest to disk j , ϕ an angle between $\hat{\mathbf{w}}_j$ and $\mathbf{d}_j - \mathbf{P}_d$, $\hat{\mathbf{v}}_j$, $\hat{\mathbf{u}}_i$, an axis system fixed on cylinder j and, finally, ϕ as an angle between $\hat{\mathbf{w}}_j$ and $\mathbf{d}_j - \mathbf{P}_d$.

$\mathbf{U}_i$ is obtained from

$$\mathbf{U}_i = \mathbf{r}_i + [(\mathbf{d}_j - \mathbf{r}_i) \cdot \hat{\mathbf{u}}_i] \hat{\mathbf{u}}_i. \quad (\text{A16})$$

First, we test the following conditions:

1. If $|\mathbf{d}_j - \mathbf{U}_i| > d$: there is no overlap.
2. If $|\mathbf{d}_j - \mathbf{U}_i| < d/2$ and $|\mathbf{d}_j - \mathbf{r}_i| > L/2$: the overlap would be a disk[−] disk kind and not a disk–rim, and therefore, we do not need to handle this condition test at this stage.
3. If $|\mathbf{d}_j - \mathbf{U}_i| \leq d/2$ and $|\mathbf{d}_j - \mathbf{r}_i| < L/2$: the two cylinders are overlapping, since the cent[er] of the disk j is within cylinder i .

Test number 3 is a sufficient, but not necessary, condition for the overlap to occur since another point can be touching cylinder j even if $\mathbf{d}_j$ is not within cylinder i .

Hence, if condition 3 is not satisfied, we have to find $\mathbf{P}_d$, the closest point in disk j to cylinder i .

Arbitrary points on the border of disk j ($\mathbf{d}$) and on the line of cylinder i ($\mathbf{c}$) are defined as

$$\mathbf{d} = \mathbf{d}_j + R \cos(\phi) \hat{\mathbf{w}}_j + R \sin(\phi) \hat{\mathbf{v}}_j, \quad (\text{A17a})$$

$$\mathbf{c} = \mathbf{r}_i + \lambda \hat{\mathbf{u}}_i, \quad (\text{A17b})$$

where $R \equiv D/2$ is the radius of the cylinders.

The square of the distance between $\mathbf{d}$ and $\mathbf{c}$ is thus

$$\begin{aligned} (\mathbf{d} - \mathbf{c})^2 &= (\mathbf{d}_j - \mathbf{r}_i)^2 + R^2 + \lambda^2 + 2R \cos \phi ((\mathbf{d}_j - \mathbf{r}_i) \cdot \hat{\mathbf{w}}_j) \\ &\quad + 2R \sin \phi ((\mathbf{d}_j - \mathbf{r}_i) \cdot \hat{\mathbf{v}}_j) - 2\lambda ((\mathbf{d}_j - \mathbf{r}_i) \cdot \hat{\mathbf{u}}_i) \\ &\quad - 2\lambda R \cos \phi (\hat{\mathbf{w}}_j \cdot \hat{\mathbf{u}}_i) - 2\lambda R \sin \phi (\hat{\mathbf{v}}_j \cdot \hat{\mathbf{u}}_i). \end{aligned} \quad (\text{A18})$$

$\mathbf{P}_c$ and $\mathbf{P}_d$ are the points that minimize Eq. (A18), therefore,

$$\lambda - r \cos \phi (\hat{\mathbf{w}}_j \cdot \hat{\mathbf{u}}_i) - r \sin \phi (\hat{\mathbf{v}}_j \cdot \hat{\mathbf{u}}_i) - ((\mathbf{d}_j - \mathbf{r}_i) \cdot \hat{\mathbf{u}}_i) = 0, \quad (\text{A19})$$

$$\begin{aligned} \sin \phi [\lambda (\hat{\mathbf{w}}_j \cdot \hat{\mathbf{u}}_i) - ((\mathbf{d}_j - \mathbf{r}_i) \cdot \hat{\mathbf{w}}_j)] \\ - \cos \phi [\lambda (\hat{\mathbf{v}}_j \cdot \hat{\mathbf{u}}_i) - ((\mathbf{d}_j - \mathbf{r}_i) \cdot \hat{\mathbf{v}}_j)] = 0. \end{aligned} \quad (\text{A20})$$

Rewriting Eq. (A20) gives

$$\frac{\sin \phi}{\cos \phi} = \frac{\lambda (\hat{\mathbf{v}}_j \cdot \hat{\mathbf{u}}_i) - ((\mathbf{d}_j - \mathbf{r}_i) \cdot \hat{\mathbf{v}}_j)}{\lambda (\hat{\mathbf{w}}_j \cdot \hat{\mathbf{u}}_i) - ((\mathbf{d}_j - \mathbf{r}_i) \cdot \hat{\mathbf{w}}_j)}. \quad (\text{A21})$$

If the numerator and denominator of Eq. (A21) are taken as the catheti of a triangle, the hypotenuse can then be found to give the expressions for $\cos \phi$ and $\sin \phi$. Once we have these expressions, they are applied to Eq. (A19), resulting in an equation for λ . Since we were not able to find an analytical solution to the previous equation, a numerical method such as the Newton–Raphson or bisection method is used to find λ . In our code, we combine both methods, running a few steps with one and a few with the other until convergence is found to machine precision.

Once $\mathbf{P}_d$ is obtained, we define $\mathbf{T} = \mathbf{P}_d - \mathbf{r}_i$, and calculate the components of $\mathbf{T}$ that are parallel $\mathbf{T}_{\parallel}$ and perpendicular $\mathbf{T}_{\perp}$ to $\hat{\mathbf{u}}_i$,

$$\mathbf{T}_{\parallel} = (\mathbf{T} \cdot \hat{\mathbf{u}}_i) \hat{\mathbf{u}}_i, \quad (\text{A22a})$$

$$\mathbf{T}_{\perp} = \mathbf{T} - \mathbf{T}_{\parallel}. \quad (\text{A22b})$$

Finally, the overlap only occurs if $|\mathbf{T}_{\parallel}| \leq L/2$ and $|\mathbf{T}_{\perp}| \leq D/2$.

DATA AVAILABILITY

The data that support the findings of this study are available within the article and its [supplementary material](#).

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Supplementary Material: Phase diagram for hard cylinders

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S1. FIGURES

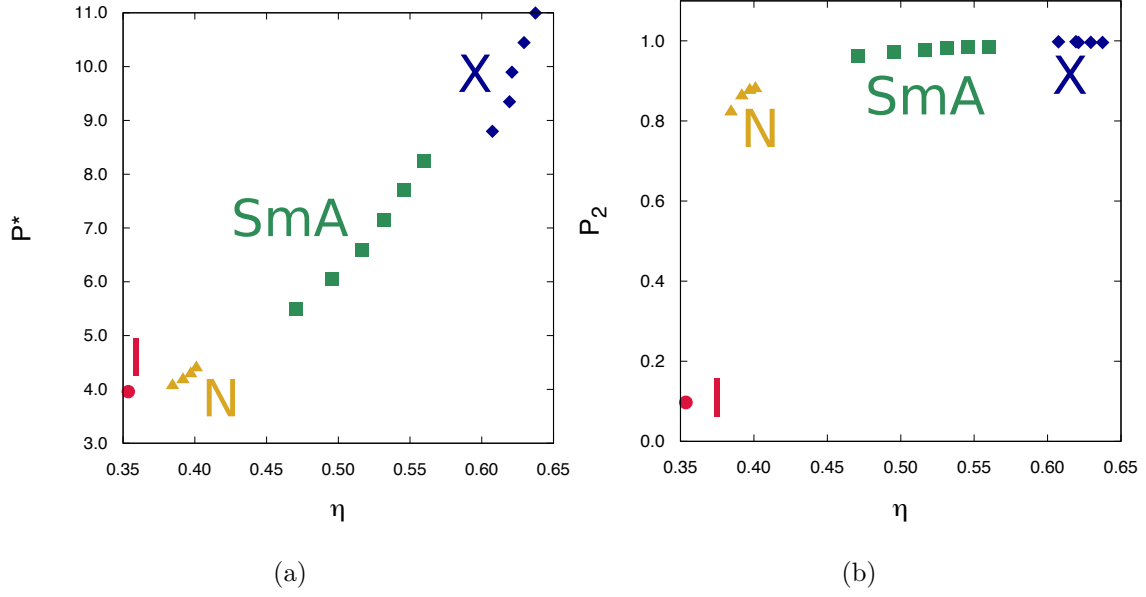
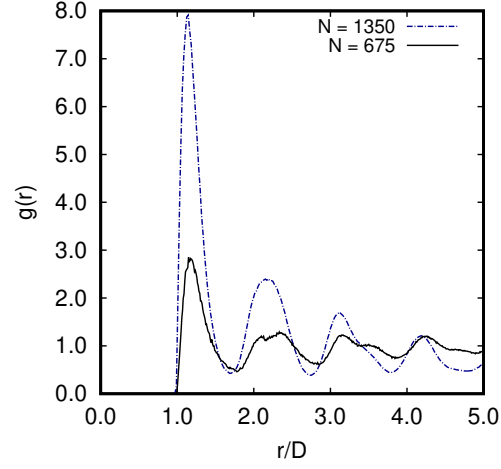
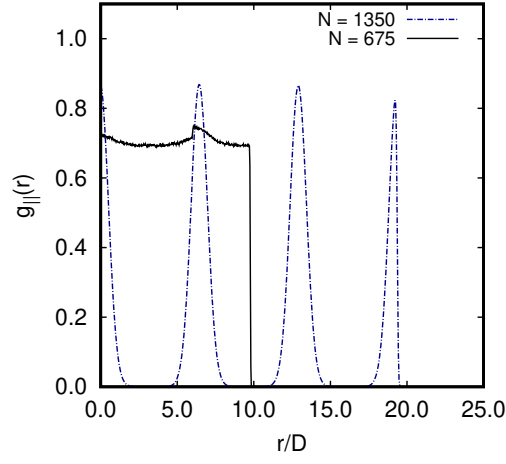


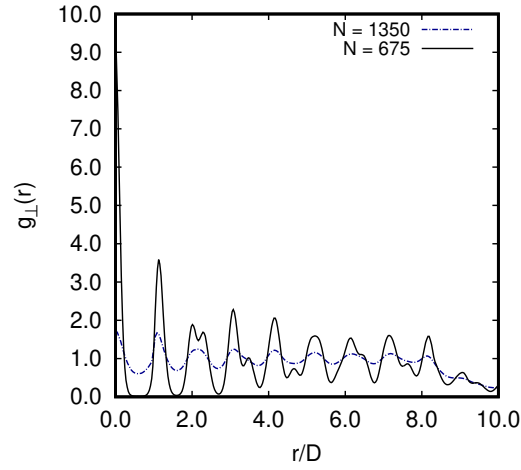
FIG. S1. (a) Reduced pressure P^* versus volume fraction η for $L/D = 7$. (b) Nematic order parameter P_2 versus volume fraction η for $L/D = 7$.



(a)



(b)



(c)

FIG. S2. Distribution functions of hard cylinders with aspect ratio $L/D = 6$ and $\eta = 0.6$ (a) $g(r)$; (b) $g_{||}(r_{||})$; (c) $g_{\perp}(r_{\perp})$. Dotted line $N = 1350$ and $P^* = 9.42$, Solid line $N = 675$ and $P^* = 8.01$.

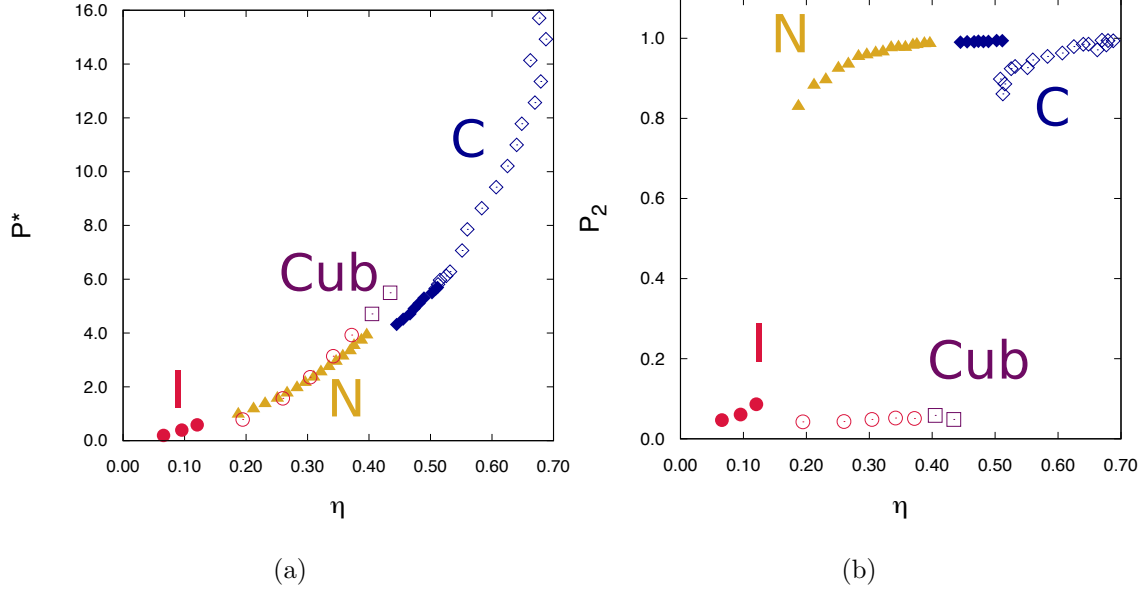


FIG. S3. (a) Reduced pressure P^* versus volume fraction η . Open symbols: $L/D = 0.2$, closed symbols: $L/D = 0.05$; (b) Nematic order parameter P_2 versus volume fraction η for both $L/D = 0.2$ and $L/D = 0.05$, with the same symbols as before.

S2. TABLES

TABLE SI. $L/D = 0.05$

P^*	η	S	ψ_6	τ	Phase
0.20	0.066 ± 0.001	0.047 ± 0.008	0.068 ± 0.007	0.178 ± 0.052	I
0.39	0.096 ± 0.001	0.061 ± 0.002	0.133 ± 0.003	0.181 ± 0.049	I
0.59	0.121 ± 0.001	0.086 ± 0.027	0.190 ± 0.006	0.185 ± 0.060	I
0.98	0.187 ± 0.001	0.830 ± 0.019	0.308 ± 0.009	0.253 ± 0.022	N
1.18	0.212 ± 0.003	0.883 ± 0.014	0.332 ± 0.009	0.193 ± 0.013	N
1.37	0.231 ± 0.004	0.896 ± 0.031	0.360 ± 0.011	0.203 ± 0.012	N
1.57	0.251 ± 0.003	0.925 ± 0.008	0.386 ± 0.008	0.178 ± 0.018	N
1.77	0.267 ± 0.001	0.935 ± 0.009	0.405 ± 0.007	0.204 ± 0.012	N
1.96	0.283 ± 0.005	0.955 ± 0.008	0.427 ± 0.006	0.113 ± 0.022	N
2.16	0.296 ± 0.004	0.959 ± 0.005	0.437 ± 0.011	0.205 ± 0.011	N
2.36	0.310 ± 0.003	0.963 ± 0.009	0.447 ± 0.013	0.194 ± 0.015	N
2.55	0.322 ± 0.001	0.966 ± 0.006	0.455 ± 0.010	0.216 ± 0.003	N
2.75	0.335 ± 0.003	0.976 ± 0.005	0.477 ± 0.009	0.176 ± 0.013	N
2.95	0.346 ± 0.004	0.978 ± 0.006	0.483 ± 0.015	0.205 ± 0.008	N
3.14	0.357 ± 0.005	0.977 ± 0.007	0.488 ± 0.010	0.198 ± 0.007	N
3.34	0.369 ± 0.005	0.983 ± 0.004	0.500 ± 0.008	0.142 ± 0.015	N
3.53	0.376 ± 0.003	0.984 ± 0.002	0.501 ± 0.005	0.172 ± 0.016	N
3.73	0.388 ± 0.005	0.986 ± 0.001	0.515 ± 0.009	0.198 ± 0.011	N
3.93	0.396 ± 0.007	0.987 ± 0.003	0.513 ± 0.010	0.158 ± 0.005	N
4.32	0.445 ± 0.007	0.990 ± 0.001	0.586 ± 0.014	0.185 ± 0.007	C
4.52	0.455 ± 0.008	0.991 ± 0.000	0.597 ± 0.017	0.210 ± 0.005	C
4.71	0.467 ± 0.006	0.992 ± 0.000	0.613 ± 0.004	0.189 ± 0.004	C
4.91	0.473 ± 0.006	0.993 ± 0.001	0.607 ± 0.016	0.195 ± 0.014	C
5.11	0.481 ± 0.007	0.992 ± 0.002	0.626 ± 0.017	0.180 ± 0.012	C
5.30	0.489 ± 0.006	0.992 ± 0.002	0.633 ± 0.020	0.200 ± 0.015	C
5.50	0.502 ± 0.006	0.994 ± 0.001	0.643 ± 0.016	0.204 ± 0.014	C
5.69	0.511 ± 0.007	0.994 ± 0.000	0.632 ± 0.012	0.208 ± 0.005	C
7.85	0.575 ± 0.001	0.999 ± 0.000	0.397 ± 0.006	0.217 ± 0.003	C

TABLE SII. $L/D = 0.20$

P^*	η	S	ψ_6	τ	Phase
0.79	0.194 ± 0.002	0.042 ± 0.004	0.285 ± 0.008	0.120 ± 0.067	I
1.57	0.260 ± 0.001	0.043 ± 0.006	0.391 ± 0.006	0.130 ± 0.050	I
2.36	0.304 ± 0.002	0.048 ± 0.011	0.434 ± 0.010	0.128 ± 0.049	I
3.14	0.342 ± 0.003	0.052 ± 0.011	0.450 ± 0.004	0.129 ± 0.043	I
3.93	0.372 ± 0.004	0.051 ± 0.012	0.460 ± 0.006	0.114 ± 0.076	I
4.71	0.405 ± 0.004	0.058 ± 0.028	0.458 ± 0.007	0.135 ± 0.029	Cub
5.50	0.434 ± 0.004	0.048 ± 0.016	0.455 ± 0.008	0.122 ± 0.062	Cub
6.28	0.532 ± 0.003	0.930 ± 0.006	0.767 ± 0.006	0.216 ± 0.004	C
7.07	0.551 ± 0.004	0.927 ± 0.007	0.788 ± 0.010	0.207 ± 0.011	C
7.85	0.560 ± 0.001	0.946 ± 0.004	0.808 ± 0.006	0.218 ± 0.002	C
8.64	0.583 ± 0.004	0.955 ± 0.006	0.822 ± 0.008	0.183 ± 0.008	C
9.42	0.607 ± 0.006	0.963 ± 0.006	0.837 ± 0.011	0.110 ± 0.008	C
10.21	0.625 ± 0.004	0.979 ± 0.003	0.840 ± 0.010	0.099 ± 0.015	C
11.00	0.640 ± 0.003	0.985 ± 0.002	0.840 ± 0.008	0.111 ± 0.006	C
11.78	0.648 ± 0.002	0.986 ± 0.001	0.856 ± 0.007	0.132 ± 0.003	C
12.57	0.670 ± 0.003	0.995 ± 0.001	0.726 ± 0.010	0.210 ± 0.009	C
13.35	0.679 ± 0.003	0.994 ± 0.001	0.795 ± 0.008	0.156 ± 0.005	C
14.14	0.662 ± 0.002	0.971 ± 0.002	0.658 ± 0.012	0.202 ± 0.002	C
14.92	0.688 ± 0.002	0.994 ± 0.000	0.858 ± 0.007	0.135 ± 0.006	C
15.71	0.677 ± 0.002	0.983 ± 0.000	0.745 ± 0.009	0.187 ± 0.006	C

TABLE SIII. $L/D = 5.00$

P^*	η	S	ψ_6	τ	Phase
0.79	0.193 ± 0.003	0.029 ± 0.005	0.002 ± 0.001	0.395 ± 0.100	I
1.18	0.229 ± 0.004	0.030 ± 0.004	0.004 ± 0.001	0.367 ± 0.128	I
1.57	0.256 ± 0.004	0.029 ± 0.002	0.007 ± 0.002	0.361 ± 0.124	I
1.96	0.280 ± 0.002	0.034 ± 0.009	0.010 ± 0.002	0.426 ± 0.153	I
2.36	0.299 ± 0.003	0.034 ± 0.007	0.015 ± 0.001	0.350 ± 0.153	I
2.75	0.317 ± 0.004	0.033 ± 0.004	0.021 ± 0.002	0.423 ± 0.149	I
3.14	0.332 ± 0.003	0.032 ± 0.010	0.028 ± 0.004	0.350 ± 0.133	I
3.53	0.348 ± 0.002	0.041 ± 0.006	0.036 ± 0.002	0.335 ± 0.192	I
3.93	0.359 ± 0.002	0.040 ± 0.029	0.045 ± 0.002	0.297 ± 0.222	I
4.32	0.372 ± 0.001	0.045 ± 0.010	0.056 ± 0.003	0.406 ± 0.229	I
4.71	0.385 ± 0.002	0.042 ± 0.010	0.071 ± 0.009	0.270 ± 0.377	I
5.11	0.397 ± 0.002	0.059 ± 0.011	0.089 ± 0.003	0.208 ± 0.098	I
5.50	0.408 ± 0.003	0.044 ± 0.015	0.118 ± 0.011	0.408 ± 0.218	I
5.89	0.480 ± 0.004	0.927 ± 0.002	0.444 ± 0.017	0.625 ± 0.077	SmA
6.28	0.500 ± 0.002	0.951 ± 0.003	0.504 ± 0.008	0.756 ± 0.088	SmA
6.68	0.515 ± 0.002	0.963 ± 0.001	0.536 ± 0.008	0.825 ± 0.039	SmA
7.07	0.526 ± 0.001	0.966 ± 0.002	0.554 ± 0.006	0.839 ± 0.010	SmA
7.46	0.537 ± 0.003	0.971 ± 0.001	0.556 ± 0.004	0.875 ± 0.012	SmA
7.85	0.549 ± 0.002	0.974 ± 0.001	0.554 ± 0.003	0.861 ± 0.042	SmA
8.25	0.561 ± 0.004	0.978 ± 0.001	0.546 ± 0.003	0.880 ± 0.025	SmA
8.64	0.567 ± 0.002	0.979 ± 0.001	0.539 ± 0.004	0.890 ± 0.032	SmA
9.03	0.603 ± 0.004	0.992 ± 0.001	0.658 ± 0.010	0.855 ± 0.022	X
9.42	0.608 ± 0.005	0.991 ± 0.001	0.638 ± 0.005	0.895 ± 0.016	X
9.82	0.617 ± 0.003	0.992 ± 0.001	0.649 ± 0.006	0.888 ± 0.011	X
10.21	0.618 ± 0.003	0.991 ± 0.001	0.628 ± 0.006	0.921 ± 0.010	X
10.60	0.633 ± 0.006	0.993 ± 0.001	0.673 ± 0.011	0.897 ± 0.034	X
11.39	0.642 ± 0.004	0.995 ± 0.000	0.687 ± 0.004	0.898 ± 0.010	X
11.78	0.650 ± 0.001	0.995 ± 0.001	0.709 ± 0.009	0.900 ± 0.005	X

TABLE SIV. $L/D = 7.00$

P^*	η	S	ψ_6	τ	Phase
3.96	0.354 ± 0.002	0.097 ± 0.031	0.043 ± 0.005	0.537 ± 0.347	I
4.07	0.384 ± 0.003	0.823 ± 0.015	0.060 ± 0.004	0.203 ± 0.005	N
4.18	0.392 ± 0.003	0.863 ± 0.016	0.065 ± 0.005	0.210 ± 0.007	N
4.29	0.397 ± 0.001	0.876 ± 0.009	0.071 ± 0.012	0.198 ± 0.008	N
4.40	0.401 ± 0.002	0.880 ± 0.009	0.075 ± 0.003	0.203 ± 0.008	N
4.95	0.442 ± 0.002	0.941 ± 0.005	0.221 ± 0.012	0.541 ± 0.045	SmA
5.50	0.471 ± 0.003	0.963 ± 0.003	0.342 ± 0.015	0.708 ± 0.032	SmA
6.05	0.495 ± 0.004	0.971 ± 0.001	0.442 ± 0.013	0.793 ± 0.016	SmA
6.60	0.517 ± 0.002	0.977 ± 0.002	0.505 ± 0.018	0.837 ± 0.061	SmA
7.15	0.532 ± 0.004	0.981 ± 0.001	0.531 ± 0.013	0.850 ± 0.026	SmA
7.70	0.546 ± 0.002	0.984 ± 0.001	0.542 ± 0.004	0.861 ± 0.050	SmA
8.25	0.560 ± 0.003	0.986 ± 0.002	0.554 ± 0.004	0.866 ± 0.033	SmA
9.90	0.621 ± 0.003	0.996 ± 0.000	0.664 ± 0.005	0.899 ± 0.003	X
10.45	0.629 ± 0.004	0.996 ± 0.001	0.677 ± 0.010	0.902 ± 0.012	X
11.00	0.637 ± 0.001	0.996 ± 0.001	0.679 ± 0.003	0.915 ± 0.011	X

TABLE SV. $L/D = 10.00$

P^*	η	S	ψ_6	τ	Phase
0.79	0.165 ± 0.001	0.024 ± 0.008	0.000 ± 0.001	0.367 ± 0.161	I
1.57	0.224 ± 0.001	0.043 ± 0.013	0.002 ± 0.001	0.273 ± 0.366	I
2.36	0.299 ± 0.042	0.804 ± 0.113	0.007 ± 0.001	0.220 ± 0.004	N
3.93	0.386 ± 0.002	0.953 ± 0.003	0.033 ± 0.004	0.217 ± 0.004	N
4.71	0.432 ± 0.002	0.971 ± 0.002	0.118 ± 0.008	0.543 ± 0.022	SmA
5.50	0.475 ± 0.001	0.982 ± 0.002	0.270 ± 0.016	0.763 ± 0.010	SmA
6.28	0.504 ± 0.002	0.986 ± 0.001	0.374 ± 0.007	0.826 ± 0.019	SmA
7.07	0.528 ± 0.002	0.989 ± 0.001	0.451 ± 0.014	0.868 ± 0.023	SmA
7.85	0.548 ± 0.002	0.991 ± 0.001	0.509 ± 0.014	0.879 ± 0.014	SmA
8.64	0.570 ± 0.002	0.993 ± 0.001	0.543 ± 0.010	0.901 ± 0.018	SmA
9.42	0.611 ± 0.001	0.998 ± 0.001	0.619 ± 0.007	0.880 ± 0.004	X
10.21	0.628 ± 0.002	0.998 ± 0.001	0.670 ± 0.004	0.900 ± 0.014	X
11.00	0.642 ± 0.001	0.998 ± 0.001	0.704 ± 0.007	0.905 ± 0.017	X
11.78	0.652 ± 0.003	0.999 ± 0.001	0.710 ± 0.011	0.912 ± 0.011	X